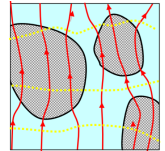
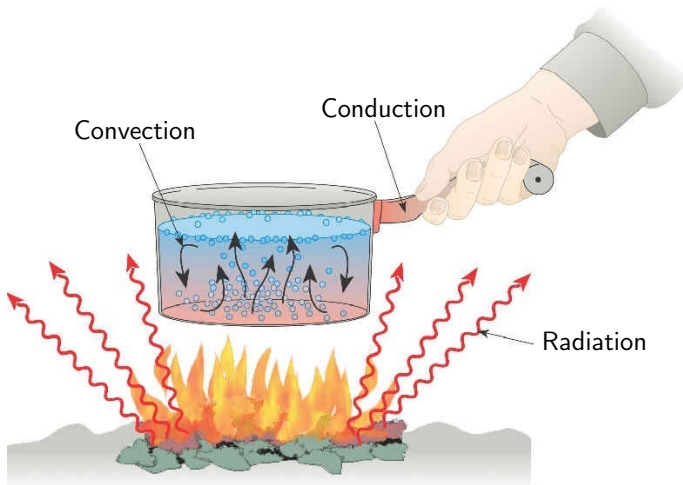


Thermal transfer in porous media



Olivier Liot Petit

- > In any media: several thermal transfer mechanisms

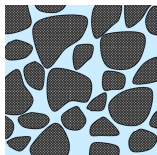


Adapted from A. Verschaere

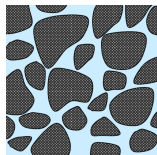
- > In porous media: co-existence of several phases with different thermal properties

Observations:

- > Several way of thermal transport
- > Different thermal properties  $\Rightarrow$  specific transfer at interfaces
- > Transport of a scalar quantity through a moving phase



**How to quantitatively describe thermal transfers in a porous media?**



Dispersion and diffusion in porous media:

- A. Derivation of thermal conduction in a porous media**
- B. Models of convection in a porous media**



### **Dispersion and diffusion in porous media**

At the end of these lectures, you should be able to:

- > cite and describe the three thermal transfer mechanisms in porous media
- > summarize the conduction thermal transfer model
- > interpret different models of equivalent conductivity
- > differentiate natural and forced convection
- > summarize the convection thermal transfer model
- > define the Rayleigh and Nusselt numbers in porous media

- > Diffusive, stationary flux
- > Flux from high temperatures to low temperatures

## Fourier's law

$$\vec{\phi} = -\bar{\lambda} \cdot \text{grad } T$$

- >  $\bar{\lambda}$ : thermal conductivity tensor  
[W.m<sup>-1</sup>.K<sup>-1</sup>]
  - >  $\vec{\phi}$ : thermal flux density vector
  - >  $T$ : temperature [K]
- 
- > Conductivity can be affected by porous structure  $\Rightarrow$  anisotropic diffusion



- > Liquid phase at rest, no heat source

**Exercise: derivation of the heat equation**



Take your device





> Liquid phase at rest, no heat source

## Exercise: derivation of the heat equation

The heat equation for conduction is...

A.  $\rho c_v \frac{\partial T}{\partial t} = \bar{\lambda} \Delta T$   
#QDLE#Q#AB\*C##

B.  $\rho c_v \frac{\partial T}{\partial t} =$   
 $\text{div}(\bar{\lambda} \cdot \vec{\text{grad}} T)$

C.  $\rho c_v \frac{\partial T}{\partial t} =$   
 $-\text{div}(\bar{\lambda} \cdot \vec{\text{grad}} T)$



- > Liquid phase at rest, no heat source

## Exercise: derivation of the heat equation

The heat equation for conduction is...

A.  $\rho c_v \frac{\partial T}{\partial t} = \bar{\lambda} \Delta T$

C.  $\rho c_v \frac{\partial T}{\partial t} = \text{div}(\bar{\lambda} \cdot \vec{\text{grad}} T)$

B.

$-\text{div}(\bar{\lambda} \cdot \vec{\text{grad}} T)$

- >  $\rho$ : density
- >  $T$ : temperature
- >  $c_v$ : constant-volume specific heat
- >  $\bar{\lambda}$  is not necessary scalar or uniform (anisotropic or inhomogeneous media)
- > Valid for both phases while at rest

## Local equations and boundary conditions

$$> (\rho c_v)_\sigma \frac{\partial T_\sigma}{\partial t} = \text{div}(\overline{\lambda}_\sigma \cdot \overrightarrow{\text{grad}} T_\sigma)$$

$$> T_\sigma = T_\alpha \text{ on } S_{\sigma\alpha}$$

$$> (\rho c_v)_\alpha \frac{\partial T_\alpha}{\partial t} = \text{div}(\overline{\lambda}_\alpha \cdot \overrightarrow{\text{grad}} T_\alpha)$$

$$> \overline{\lambda}_\sigma \cdot \overrightarrow{\text{grad}} T_\sigma \cdot \vec{n}_{\sigma\alpha} = \overline{\lambda}_\alpha \cdot \overrightarrow{\text{grad}} T_\alpha \cdot \vec{n}_{\sigma\alpha}$$

Remind – volume averages:

$$> \text{Surface average: } \langle \Phi_\alpha \rangle = \frac{1}{V} \int_{V_\alpha} \Phi_\alpha dV$$

$$> \text{Intrinsic average: } \langle \Phi_\alpha \rangle^\alpha = \frac{1}{V_\alpha} \int_{V_\alpha} \Phi_\alpha dV$$

Remind – volume averaging theorems:

$$> \text{Gradient: } \langle \overrightarrow{\text{grad}} \Phi_\alpha \rangle = \overrightarrow{\text{grad}} \langle \Phi_\alpha \rangle + \frac{1}{V} \int_{S_{\alpha\sigma}} \Phi_\alpha \vec{n}_{\alpha\sigma} dS$$

$$> \text{Divergence: } \langle \text{div} \overrightarrow{\Phi}_\alpha \rangle = \text{div} \langle \overrightarrow{\Phi}_\alpha \rangle + \frac{1}{V} \int_{S_{\alpha\sigma}} \overrightarrow{\Phi}_\alpha \cdot \vec{n}_{\alpha\sigma} dS$$

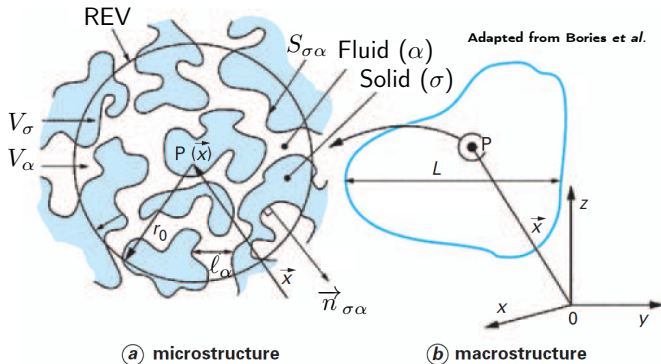
$$> \text{Time-variation: } \left\langle \frac{\partial \Phi_\alpha}{\partial t} \right\rangle = \frac{\partial \langle \Phi_\alpha \rangle}{\partial t} - \frac{1}{V} \int_{S_{\alpha\sigma}} \Phi_\alpha \vec{W} \cdot \vec{n}_{\alpha\sigma} dS$$

■  $\vec{n}_{\alpha\sigma}$ : normal vector to  $\sigma$  and  $\alpha$  interface

■  $S_{\alpha\sigma}$ :  $\sigma$  and  $\alpha$  interface

■  $\vec{W}$ : displacement velocity vector of interface  $S_{\alpha\sigma}$

- > Rigid porous structure and only one non-solid phase  $\vec{W} = \vec{0}$



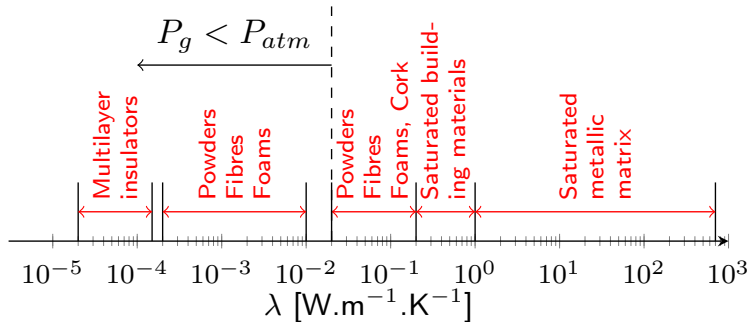
## Volume averaged heat equation

$$(\rho c_v)^* \frac{\partial T}{\partial t} = \text{div}(\bar{\lambda} \cdot \text{grad} T)$$

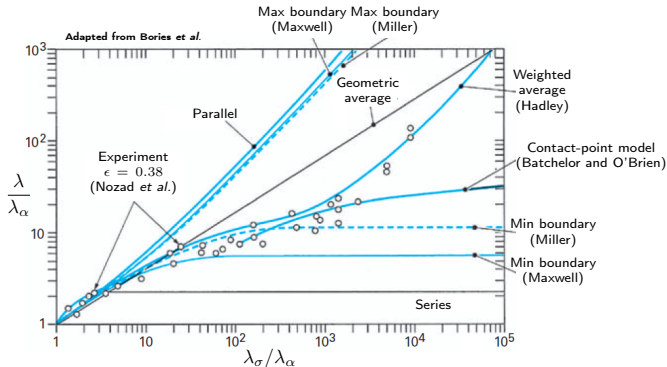
- > Effective calorific capacity:  
 $(\rho c_v)^* = \epsilon(\rho c_v)_\alpha + (1 - \epsilon)(\rho c_v)_\sigma$

- > Effective conductivity:  $\bar{\lambda} = (\epsilon \bar{\lambda}_\alpha + (1 - \epsilon) \bar{\lambda}_\sigma) + \frac{\bar{\lambda}_\alpha - \bar{\lambda}_\sigma}{V} \cdot \int_{S_{\alpha\sigma}} \vec{b} \cdot \vec{n}_{\alpha\sigma} dS$

> Some orders of magnitude



- > Several models (Maxwell, Miller, Hadley, Batchelor-O'Brien, ...)

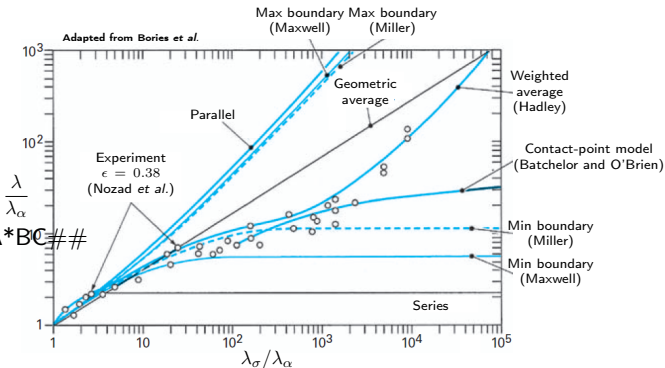


**Exercise: derivation of the effective conductivity for simple arrangements**

Take your device



> Several models (Maxwell, Miller, Hadley, Batchelor-O'Brien, ...)



**Exercise: derivation of the effective conductivity for simple arrangements**

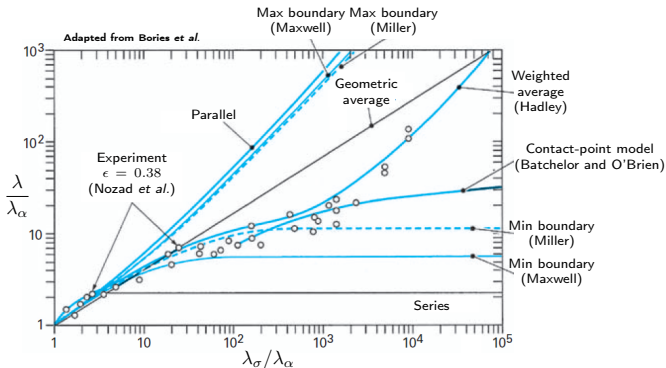
The effective conductivity for the parallel arrangement is...

A.  $\lambda = \lambda_\alpha \left( \epsilon + (1 - \epsilon) \frac{\lambda_\sigma}{\lambda_\alpha} \right)$

B.  $\lambda = \lambda_\alpha \left( \epsilon + (1 - \epsilon) \frac{\lambda_\alpha}{\lambda_\sigma} \right)$

C.  $\lambda = \lambda_\alpha \left( \epsilon + \frac{\lambda_\sigma}{\lambda_\alpha} \right)$

- > Several models (Maxwell, Miller, Hadley, Batchelor-O'Brien, ...)



**Exercise: derivation of the effective conductivity for simple arrangements**

The effective conductivity for the parallel arrangement is...

A. 
$$\lambda = \lambda_\alpha \left( \epsilon + (1 - \epsilon) \frac{\lambda_\sigma}{\lambda_\alpha} \right)$$

B. 
$$\lambda = \lambda_\alpha \left( \epsilon + (1 - \epsilon) \frac{\lambda_\alpha}{\lambda_\sigma} \right)$$

C. 
$$\lambda = \lambda_\alpha \left( \epsilon + \frac{\lambda_\sigma}{\lambda_\alpha} \right)$$

- > Fluid is moving  $\Rightarrow$  additional transport of heat
- > Two kind of convections:

■ Natural convection

■ Forced convection



- > Natural: driven only by density differences
- > Forced: external wind imposed

- > Hypothesis: local thermal equilibrium:  $T = \langle T_\sigma \rangle^\sigma = \langle T_\alpha \rangle^\alpha$
- > Darcy's law valid, no inertia, volume averaging

## Volume averaged heat equation with convective part

$$(\rho c_v)^* \frac{\partial T}{\partial t} + (\rho c_v)_\alpha \langle \vec{v} \rangle \cdot \overrightarrow{\text{grad}} T = \text{div} \left[ (\bar{\lambda} + \bar{\lambda}_d) \cdot \overrightarrow{\text{grad}} T \right]$$

$$\langle \vec{v}_\alpha \rangle = -\frac{\bar{k}}{\eta} (\overrightarrow{\text{grad}} \langle P_\alpha \rangle^\alpha - \rho_\alpha \vec{g}) \quad \text{and} \quad \epsilon \frac{\partial \rho_\alpha}{\partial t} + \text{div}(\rho_\alpha \langle \vec{v}_\alpha \rangle) = 0$$

- >  $\bar{\lambda}_d$ : effective thermal conductivity tensor due to dispersion

## Diffusivity tensor

$$\bar{D} = \frac{\bar{\lambda} + \bar{\lambda}_d}{(\rho c_v)_\alpha} = \frac{\bar{\lambda}}{(\rho c_v)_\alpha} + \bar{D}_d$$

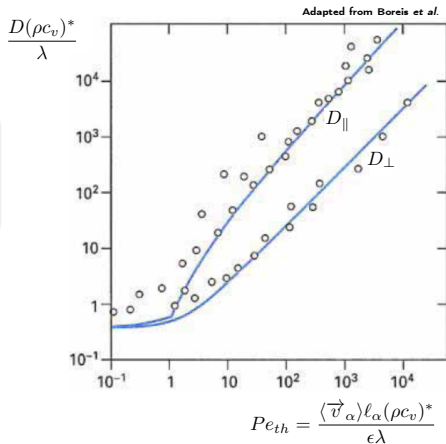
- > Two components: longitudinal ( $D_{\parallel}$ ) and transverse ( $D_{\perp}$ )

## Thermal Péclet number

$$Pe_{th} = \frac{\text{convection}}{\text{conduction}} = \frac{\langle \vec{v}_\alpha \rangle l_\alpha (\rho c_v)^*}{\epsilon \lambda}$$

> Analog to Péclet number for dispersion

> If only diffusion,  $D = \frac{\lambda}{(\rho c_v)^*}$





- > Dependence of  $\rho_\alpha$  with  $T$ :  $\rho_\alpha(T) = \rho_\alpha(T_0)(1 - \beta(T - T_0))$
- $\beta$ : thermal expansivity coefficient of the fluid

**Exercise: dimensionless numbers in natural convection**

Take your device



- > Dependence of  $\rho_\alpha$  with  $T$ :  $\rho_\alpha(T) = \rho_\alpha(T_0)(1 - \beta(T - T_0))$ 
  - $\beta$ : thermal expansivity coefficient of the fluid

## Exercise: dimensionless numbers in natural convection

The Rayleigh number expression is...

A.  $Ra = \frac{gdk(T_1 - T_2)}{D\nu}$

B.  $Ra = \frac{\beta g d^3 k (T_1 - T_2)}{D\nu}$

C.  $Ra = \frac{\beta g d k (T_1 - T_2)}{D\nu}$

> Dependence of  $\rho_\alpha$  with  $T$ :  $\rho_\alpha(T) = \rho_\alpha(T_0)(1 - \beta(T - T_0))$

■  $\beta$ : thermal expansivity coefficient of the fluid

### Exercise: dimensionless numbers in natural convection

The Rayleigh number expression is...

$$\text{A. } Ra = \frac{gdk(T_1 - T_2)}{\beta D\nu} \quad \text{B. } Ra = \frac{\beta g d^3 k(T_1 - T_2)}{D\nu} \quad \text{C. } Ra = \frac{\beta g d k(T_1 - T_2)}{D\nu}$$

> Rayleigh number: comparison between convection “engines” and “breaks”

> “Prandtl” number:  $Pr = \frac{\nu d^2}{kD}$

Thermal flux;

> Nusselt number:  $Nu = \frac{\text{total heat flux}}{\text{conductive heat flux}}$

## > Heat flux versus thermal forcing

